DETERMINATION OF STOL AIR TERMINAL TRAFFIC CAPACITY THROUGH USE OF COMPUTER SIMULATION

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THESIS

DETERMINATION OF STOL AIR TERMINAL TRAFFIC CAPACITY THROUGH USE OF COMPUTER SIMULATION

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September 1971

IN THE THEM SCHOOL

Determination of STOL Air Terminal Traffic Capacity Through Use of Computer Simulation

by

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Submitted in partial fulfillment of the requirements for the degree of

MASTER OF SCIENCE IN OPERATIONS RESEARCH

from the

NAVAL POSTGRADUATE SCHOOL September 1971 Ph 5717

ABSTRACT

The capacity of an air terminal for Short Takeoff and Landing air-craft is analyzed. The terminal is considered to be operating as part of an intra-urban air rapid transit system. The air traffic flow through the terminal is modeled by a computer simulation written in both the FORTRAN IV and GPSS languages. The model is used to solve the traffic capacity problem under two sets of traffic control rules. In the first case, existing FAA rules, which require 3 miles separation between arrivals and 2 miles between an arrival and a departure, are used. In a second case, the rules are 2 miles between arrivals and 1 mile between an arrival and a departure. A detailed description of the model is presented so that others might use the model.



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I. INTRODUCTION

One of the many problems facing our cities today is the lack of effective and economically feasible rapid transit systems. Solutions to this problem cannot be thought of in terms of today's hardware and technology because of the long lead time required for development of complex rapid transit systems. In fact, today one must consider systems for operation five or ten years in the future.

One system that is currently being examined is based on the use of Short Takeoff and Landing (STOL) aircraft in this very short haul intraurban market. This type of transportation system may be suitable for an urban area such as the San Francisco Bay area. It would complement rather than replace existing systems, such as San Francisco's BART. To the extent possible, the STOL system would use existing facilities. Where no air terminals now exist, such as in downtown San Francisco, terminals would be built especially for the STOL system.

The system is envisioned to operate more like a bus line than an air line. There would be no cabin attendants and stops at terminals would be a matter of minutes instead of hours. Only one basic type of aircraft would be used and the system would be operated under a local monopoly, probably by a municipally owned company.

The National Aeronautics and Space Administration has initiated both in-house and contract studies of the STOL rapid transit system.



NASA examined the economics of the system [1], and the system was found to be economically feasible. Reassured that the idea had merit, NASA let contracts for a detailed system design to the Boeing corporation. The Boeing study proposed an aircraft to be used in the system and a terminal design and placement scheme. [2] The STOL port proposed had a single runway with multiple passenger gates. It was to be used only by the STOL system with no other traffic allowed.

Boeing performed an economic analysis of their system proposal and found it to be economically feasible under the proper assumptions. The critical economic areas were the fixed costs of construction and operation, and the costs of unproductive ground and holding pattern time of the aircraft. [2] All of these costs are directly related since a greater amount of unproductive aircraft time requires more aircraft to satisfy a given demand than would be required if the unproductive time were short. The higher number of aircraft would require more terminal facilities to handle them. The cost of having to obtain and operate the increased number of terminals and aircraft could make the system economically unsound. Thus it is important to have both aircraft and terminals operating efficiently to minimize the number of each required to operate the system.



II. STATEMENT OF THE PROBLEM

The matter of facility capacity seems to be an important key to the potential success of the system. This paper presents the development of a model which can be used to determine STOL terminal traffic capacity in the context of the rapid transit system described above.

Given a particular set of assumptions, a measure of capacity will be defined and capacity determined under two sets of traffic control rules. The two solutions will be made to demonstrate the effect on capacity of allowing reduced aircraft separation.

First the problem will be solved using existing FAA traffic separation rules of 3 miles between consecutive arrivals and 2 miles between an arrival and a departure. The problem will then be solved using separation requirements of 2 miles between consecutive arrivals and 1 mile between an arrival and a departure. This latter set of separation requirements reflect rule changes that may result from the use of more precise navigation and air traffic control equipment.



III. SOLUTION TECHNIQUE

The economic success of the STOL rapid transit system depends heavily on the rapid and efficient cycling of aircraft through the terminals. The consequences of an inaccurate capacity figure therefore make an educated guess, or trial and error solution, unacceptable, since long aircraft delays caused by overloaded terminals or idle facilities caused by under utilized assets would prove disasterous to the system budget.

Computer simulation was chosen as the solution method in light of the necessity of a solution and the obstacles posed by direct analytical techniques. The interdependencies between various events in the system would make direct solution an impossible task. If the dependencies and distributions involved were simplified to the point that direct mathematical solution was possible, the model resulting would probably be only a gross representation of the system.

The simulation model described in the following sections was used in the problem solution. Five hours of simulated time were simulated to examine the period covering evening rush hour, this being the time of heaviest traffic. The model was run for two hours of simulated time at 1/2 peak flow. The traffic flow rate was then increased over a period of 90 minutes to peak flow and held there for one hour of simulated time. The model then simulated another 30 minutes at a traffic flow of 1/3 peak.



Data was examined for the final 3 hours of the 5 simulated hours. The peak flow was adjusted until the traffic capacity was found. The criterion used to define capacity was the expected delay time for those aircraft which had to wait to start their approach. This was estimated using the average holding pattern time. When the expected delay time for those aircraft that had to wait reached 3 minutes, the airport was considered to be at capacity. This admittedly somewhat arbitrary criterion was chosen because it represents the author's opinion of the maximum amount of time a traffic controller could be expected to be able to delay an arrival by indirect routing - hence it is the point at which an arrival would have to enter a holding pattern.



IV. ASSUMPTIONS

A. LIST OF ASSUMPTIONS

The assumptions that were made in the solution of the problem were:

- 1. The aircraft involved is a multi-engine STOL aircraft with fast load/unload capability.
- 2. The aerodynamic stall speed is 60 MPH in the landing configuration.
- 3. The speed the aircraft flies on the approach is normally distributed with mean 82.3 MPH and standard deviation of 5.04 MPH.
- 4. The landing speed is normally distributed with mean 77 MPH and standard deviation 4.25 MPH.
- 5. The aircraft decelerates after landing at a constant rate of 10 ft/sec² until a speed of 10 MPH is reached. At that time, the aircraft turns off the runway and is clear in 5 seconds.
- 6. The distribution of time between arrivals is exponential and all arrivals are independent.
- 7. Taxi time between the runway and the gates is 1.5 minutes for arrivals and departures.
 - 8. Gate time is exponentially distributed with a mean of 3 minutes.
- 9. The time required to position the aircraft in position for takeoff on the runway is .25 minutes.



- 10. The take-off is modeled as a constant acceleration from a standing start at the rate of 10 ft/sec², until a speed of 77 MPH is reached.
 - 11. The terminal has an approach course that is 9 miles long.
- 12. 13 miles must be flown back to the start of the approach course if a go-around (or wave-off) is necessary.
- 13. The aircraft is capable of executing a safe wave-off from any point on the approach course greater than 0.1 miles from the landing point.
 - 14. The terminal is equipped with 3 passenger gates.
 - 15. The weather is good with no wind.

B. JUSTIFICATION OF ASSUMPTIONS

This section is included to explain the reasons for the assumptions made in the problem solution.

- 1. The aircraft was modeled after the proposal made by the Boeing corporation. [2]
- 2. The speed distributions for both the approach speed and landing speed were based on a study of speed distributions of present day passenger jets [3], and the premise that the STOL aircraft will be able to be flown as consistently near designed approach speed as present day commercial aircraft. There is reason to believe they will in fact be easier to fly than today's jets.



- 3. The inter arrival time assumption is based on studies of actual arrivals at commercial airports [4,5,6]. One may doubt the validity of drawing an analogy between contemporary commercial airports, with many independent (in the statistical sense) airlines, and the one company STOL port. However a parallel situation does exist. Instead of different airlines, we have aircraft on different routes in the system. If one considers each route as a different line, the exact same traffic situation exists at the STOL port and a commercial air port.
- 4. The gate time distribution assumption is based on the characteristics of similar types of short stop systems [4].



V. SENSITIVITY ANALYSIS

This section is included to indicate the sensitivity of the solution to the assumptions made.

The speed distribution assumption is conservative. The previous section indicated that the normality assumption would probably result in speeds more variable than would actually exist. This is stated to be conservative because a smaller variation in speeds than that assumed would result in a larger peak flow at capacity. This happens because the traffic separation is attained at the start of the approach. If two consecutive arrivals have different approach speeds and the faster one follows the slower one, the second may be too close behind the first at landing. If this happens, the first aircraft will not be clear of the runway and the second will have to go around.

The solution is entirely dependent on the mean approach speed assumed. Since the separation required is specified as distance between aircraft (rather than time between aircraft), aircraft with faster approach speeds will be able to attain this distance in less time than slower aircraft. The wind plays a role in this also, since the ground speed actually determines the time needed to get the required spacing. An indication of the effect of ground speed can be seen by noting that the time needed to get the approach separation is a linear function of the ground speed. At the assumed ground speed of 82.3 MPH, a capacity of



22 aircraft per hour can be handled using the 3 mile separation rule.

Applying the ratio of peak flow to speed, one can predict a peak capacity
of 24 aircraft per hour at a speed of 92 MPH, and 19 per hour at 72 MPH.

The selection of the landing speed and deceleration assumption become critical only when the time required for an aircraft to clear the runway after landing is so great that there is no opportunity to insert a departure between two arrivals. Naturally the amount of time required for a departure is as important as the time needed for a landing. The time needed for a departure to taxi into position for takeoff is not critical since this can be done while the previous arrival is decelerating. What is required then is that the time between arrivals be such that a deceleration from landing speed to taxi speed and an acceleration to takeoff speed can occur. Looking at the mean speeds involved, we find that a landing followed by a takeoff takes about 25 seconds. The average time between arrivals (using 2 miles separation and 82 MPH) is 88 seconds. There is obviously a lot of slack time available, which means that the landing and takeoff procedures are not critical to the flow rate.

Taxi time has no effect on the waiting time and simply adds on to the total cycle time. Thus as far as the capacity of the terminal is concerned, the taxi time is really immaterial.

The gate time could have an effect on the solution. With the 3 minute mean time assumed, the gate queue was normally empty for all flow rates tested. Obviously, the amount of gate time available (number of gates multiplied by the time period being considered) can be such that



the gates become a bottleneck, the solution then would have to consider waiting time at the gates as well as at the holding pattern.

The weather assumption is not important. The model operates air craft under Instrument Flight Rules. These procedures will operate the same regardless of the actual weather, unless the weather is so bad it forces closure of the terminal. It is true that bad weather results in higher landing speeds and lower deceleration rates, but since there is so much slack available in the landing and roll out phase, these longer runway times will have no effect on the solution obtained.



VI. ANALYSIS OF DATA

As has been stated, the statistic used to indicate capacity was average conditional waiting time. If this time was 3 minutes or greater the airport was considered over capacity. The model operates on the basis of abstract time units, with the interpretation in this solution being that 1 time unit equals 5 seconds. Thus the question was really to find the maximum flow rate that resulted in an expected conditional waiting time of 36 time units or less. As a preliminary step, based on the Central Limit Theorum, the assumption was made that the average conditional waiting time was distributed normally with mean equal to the true mean of the waiting time and variance unknown.

With the assumptions stated above, the following procedure was used to determine the maximum peak flow rate that resulted in a mean conditional waiting time of 36 time units or less.

- 1. A value of peak flow was picked and the model run for 10 replications.
- 2. a. If the average value of the mean conditional waiting time was greater than 36, a test of hypothesis using the 95 percentile point of the "t" distribution was made. Ho was that the true mean was less than 36, Ha that the true mean was greater than or equal to 36.
- b. If the average of the mean conditional waiting time was less than 36, the test of hypothesis was made with Ho being that the



true mean was greater than 36, and Ha that the true mean was less than or equal to 36.

- 3. a. If Ho was not rejected, more data was taken and pooled with the previous data. The test of hypothesis procedure described above was repeated.
- b. If Ho was rejected, the peak flow rate was adjusted. If the average of the sample tested was greater than 36, the peak was decreased. If the average of the sample just tested was less than 36, the peak flow rate was increased. The model was run for 10 replications at the new peak flow rate and the above procedure repeated starting at step 2.

The flow chart of Figure 1 illustrates the procedure just described. This search and test procedure was used to try to minimize the computer time needed to solve the problem. Since the actual flow rate capacity was not known within 10 increments, testing all reasonable possibilities, using a sample size large enough to insure a desired confidence level, would have been an expensive procedure. As it was, approximately 45 minutes of computer time was required to get the data that was used.

A disadvantage of this procedure is that, due to the sequential nature of the data collection and hypothesis testing, it cannot be said that the hypotheses were tested at the 95% level, even though the 95 percentile point of the "t" distribution was used to define the critical regions.

Lindgren [7] presents a discussion of the problems associated with sequential sampling. The true value of the type I error in this case (the probability of rejecting a true Ho) is greater than 5%. Unfortunately,



it is probably beyond calculation. The difficulty of calculation is compounded by the fact that the sequential tests were not of the same sample size. Often a different number of data points resulted from different batches of runs. This was a phenomenon peculiar to the monitor system of the computer installation where the model was run. If the run time exceeded a certain real time limit, the run was terminated at that point.



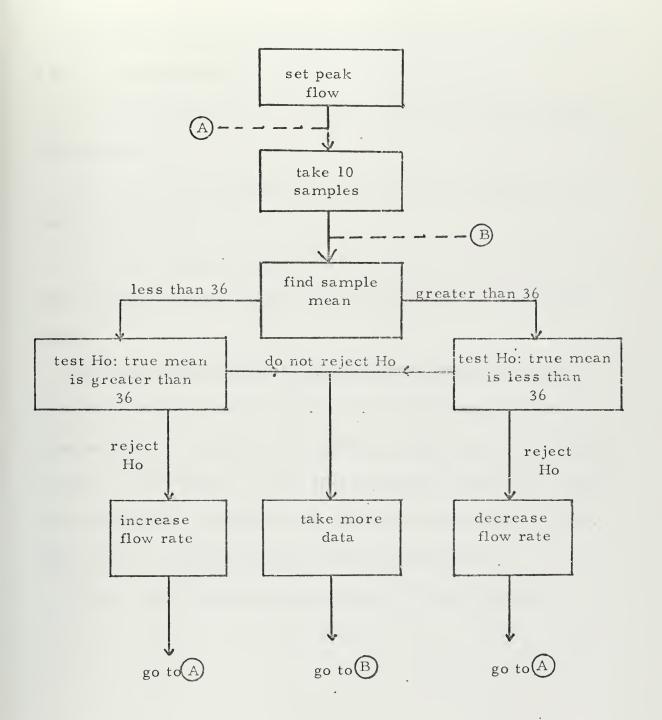


FIGURE I. ANALYSIS PROCEDURE



VII. RESULTS

The model was run under the conditions as stated. For each run of 5 hours of simulated time, the following was recorded:

- 1. The proportion of aircraft that did not have to wait to start their approach.
- 2. The average waiting time for those aircraft that had to wait to start their approach.
- 3. The average time for an aircraft to cycle through the terminal, measured from arrival at the start of the approach to completion of take-off.

The three scts of data were kept in hopes of finding a suitable correlation between them. The criterion decided upon to measure capacity, that is, the expected conditional waiting time, proved highly variable. Unfortunately, no precise correlation could be found which would allow the use of another measure to indicate that the desired delay limit of 3 minutes average delay had been reached.

Tables 1 and 2 contain a summary of the results obtained.



TABLE I SUMMARY OF RESULTS

3 MILES BETWEEN ARRIVALS, 2 MILES BETWEEN ARRIVALS AND DEPARTURES

R	N	PNW	M	S	С	Hg	Hl
25	10	.28	54.10	20.21	202.76		R
24	- 11	. 33	45.20	19.93	197.14		R
23	99	.38	39.31	21.75	187.54		R
22	105	. 43	32.72	15.71	179.74	R	
21	48	. 46	31.88	17.77	178.24	R	

R = Peak arrival rate in aircraft per hour.

N = Number of replications on which figures are based.

PNW = Average proportion of aircraft that did not have to wait.

M = Average conditional waiting time, in model time units.

S = The sample standard deviation of the conditional waiting time, in model time units.

C = The average cycle time, in model time units.

Hg : An "R" in this column indicates that the hypothesis "the true mean is greater than 36" was rejected.

H1 : An "R" in this column indicates that the hypothesis "the true mean is less than 36" was rejected.



TABLE 2
SUMMARY OF RESULTS

2 MILES BETWEEN ARRIVALS, 1 MILE BETWEEN ARRIVALS AND DEPARTURES

R	N	PNW	M	S	С	Hg	Hl
36	74	.30	38.23	21.91	192.48		R
34	167	. 35	34.96	25.22	187.28	\$¦<	*
33	123	. 36	32,54	19.50	185.30	R	
32	50	. 42	26.14	14.99	178.87	R	

Column headings in this table are the same as those used in Table I.

* The flow rate of 34 per hour could not be resolved. That is, the hypothesis that the true mean was greater than 36 could not be rejected, even with the large number of data points obtained. In view of the large sample variance at this level, and the closeness of the sample mean to 36, it was decided to abandon this flow rate and be satisfied with knowing that the flow rate just below it was under capacity, while the one above it was over capacity.

The flow rate of 35 per hour is omitted because it could not be represented by an integer number of time units of 5 seconds width.



VIII. CONCLUSIONS

It was concluded that under existing FAA traffic separation rules, the capacity of the terminal was a peak flow rate of 22 aircraft per hour. Under the revised separation requirements of 2 miles between arrivals and 1 mile between an arrival and a departure, a peak flow of 33 aircraft per hour can be handled.

There is a significant advantage to be gained from allowing the closer spacing. It would certainly be worth while to carefully examine the separation rules to be applied. It is too expensive in terms of lost capacity to require unnecessary distance between aircraft.

The capacity figures resulting from this solution are considerably more pessimistic than those used in the Boeing study. Their assumptions resulted in a much more disciplined arrival rule than the Poisson process assumed here. In fact, they assumed that the aircraft arrived at the Initial Approach Fix already properly spaced for the approach [2]. As a result, they were able to sustain a flow rate of 28 aircraft per hour under existing rules, and a flow rate of 41 aircraft per hour under the 2 mile - 1 mile rules.



IX. MODEL DESCRIPTION

The model was designed to represent the specific scenario of a STOL terminal operating in the environment of an intra-urban rapid transit system. As a result, the following assumptions are built into the model and cannot be changed without re-writing the program.

- 1. The model considered traffic to be homogenious. In this case, homogenious applies both to the aircraft type involved and to the method of operation. All aircraft are considered under positive radar control and operating under instrument flight rules (IFR).
- 2. The terminal modeled has a single runway with a single approach course from the holding pattern to the runway.
 - 3. The holding pattern is at the initial approach fix (IAF).
 - 4. All queues are of the first-in-first-out type.
 - 5. Arrivals are given priority over departures.
- 6. Aircraft that have had to go around on an approach are given priority for another approach over other aircraft in the holding pattern.

The traffic flow in the model is as indicated in Figure 2. Figure 3 shows the physical system that is modeled.



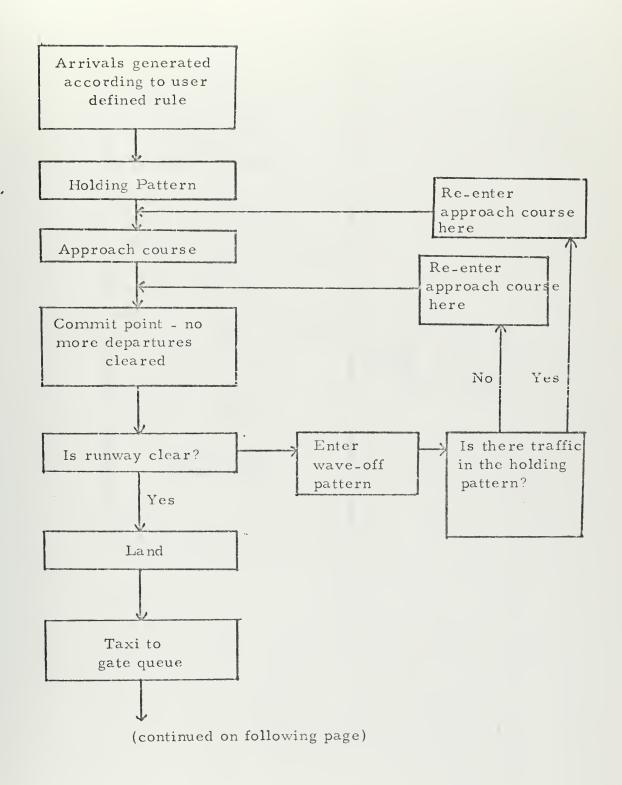


FIGURE 2. TRAFFIC FLOW



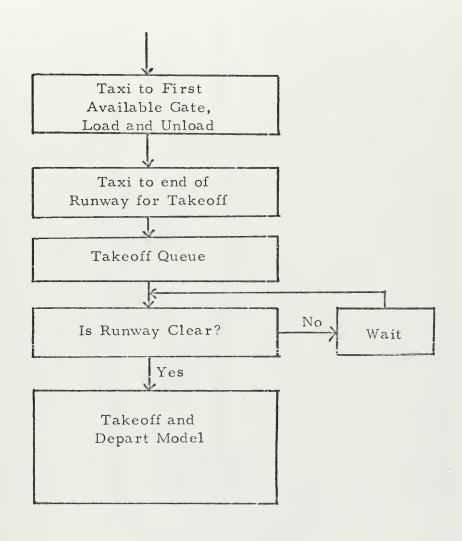


FIGURE 2. (continued)



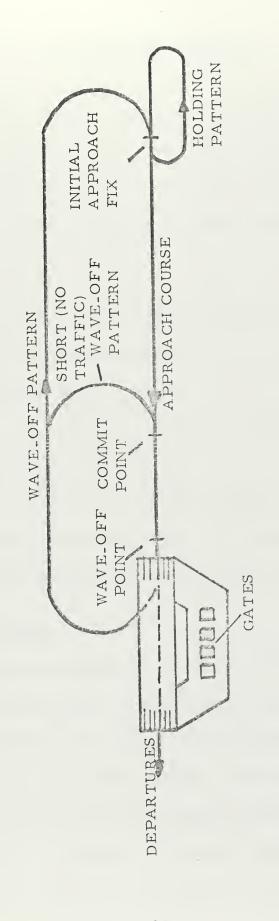


FIGURE 3. TYPICAL STOL TERMINAL ASSUMED



X. THE GPSS PROGRAM

The simulation was written using General Purpose Simulation

System (GPSS). This system generates entities and moves them through
a sequence of queues and facilities according to user defined rules. It
uses abstract time units to measure flow rates and delay times.

A. GPSS ANALOGIES

The analogies that are used in the GPSS model are as follows:

- 1. Queue 1 represents the holding pattern, queue 3 the gate queue, and queue 4 the takeoff queue.
- 2. Facility 1 represents the approach course, facility 2 the runway, and facility 21 the runway threshold.
- 3. Storage 1 represents the passenger gates, with the storage capacity determining the number of gates to be simulated.
 - 4. Each GPSS entity represents an aircraft in the system.

B. GPSS FUNCTIONS

In order to use the model, one must have a basic knowledge of GPSS functions since they are used to describe transit and delay time probability distributions. To define a function, the user must input a set of ordered pairs to the GPSS program. The program interprets the first number of each ordered pair as the independent variable, and the second as the dependent variable. The entire function is approximated by linear interpolation between the poin's described.



The GPSS program generates a uniform random variate on the interval 0 to 1 (or 0 to 1000) to 3 significant figures. By using this number as the independent variable, a function value is obtained from the user defined function. This value is then multiplied by the mean of the distribution in question to get a realization from the distribution.

In other words, the function defined represents a mapping from a uniform distribution to the desired cumulative probability distribution, normalized so that its mean is 1.

The exact mechanics and form for inputting the ordered pairs will be described in section XII.

C. GPSS OUTPUT

The GPSS output is organized into sections as follows: (the reader may find it helpful to refer to the GPSS output from the sample run in Appendix B).

- 1. Source listing of the GPSS deck. In this listing each operational card is assigned a block number and each card in the program is assigned a card number by the compiler. It will be noted that these program assigned numbers bear no relation to the card numbers punched in columns 78-80 of the source deck.
- 2. A partially compiled source listing (this listing is omitted in Appendix B).
- 3. The flow summary. This is the first of the statistical output data from the run. This summary is a count of the total number of



entities that have moved through each block, as well as the number that were present in the block at the end of the run. Note that if statistics are kept from other than the start of the run, the total shown for each block is summed only over the time for which statistics were kept.

- 4. The runway utilization statistics. Three values are shown here. The average utilization is computed as the proportion of time the runway was occupied. The number of entries is a count of the number of operations, takeoffs and landings, that occurred on the runway. The average time per transaction is the average time each runway operation took, in GPSS time units.
- 5. The runway threshold utilization statistics. The data in this section is computed in the same manner as the runway utilization statistics.
- 6. The gate statistics. The capacity simply indicates the number of gates that were simulated. The average contents shows the average number of aircraft that were at the gates. The average utilization is the proportion of available gate time that was used. The average time per transaction is computed as the average time an aircraft remained at the gate, in GPSS time units. The current contents and maximum contents are self explanatory.
- 7. The queue statistics. These are self explanatory except for the zero entity concept. A zero entity is one which did not have to wait in the queue, but simply passed through. The \$AVERAGE TIME/TRANS column shows the average time each entity had to wait in the queue, not counting zero entities.



8. Table of transit times. This is a tabulation of the total time each aircraft took to transit the model, in GPSS time units. The table structure, that is the range and increment size, is user defined. The overflow portion of the table includes all values greater than the table upper bound. All intervals in the table have as their lower bound the upper bound of the previous interval. The first interval has zero as its lower bound.



XI. THE FORTRAN PROGRAM

The FORTRAN section of the model is used solely as a preprocessor to convert input data to a form acceptable to the GPSS
program. It accepts inputs in a convenient form and units, such as
MPH, miles and ft/sec². It outputs printed output for the information
of the user, and punched output to be included in the GPSS deck.

A. FORTRAN INPUTS

All inputs to the FORTRAN program are on punched cards. Appendix B shows a sample input deck. Inputs fall into two types, required and optional. Naturally, all required inputs must be assigned values for each run. The normal FORTRAN convention relating to variable types has been followed, all variables are real (decimal) numbers except those whose names start with the letters I, J, K, L, M, N, or O. Input variables which are real numbers must have a decimal point supplied, even if the value assigned is a whole number. Integer variables must not have decimal points included.

The first character of each card of the input deck must be punched starting in column 2, while the last character on each card must be before column 72. The first characters on card 1 of the input deck must be an ampersand followed by the word INPUT, followed by at least one blank.



A variable is assigned a value by punching the variable name, an equal sign, its value and a comma. An example is: ARRT=5.3, . After the last comma on the last card, an ampersand followed by the word END must be punched.

As many cards as are necessary may be used. Spacing between variables is unimportant. The last character on all cards except the last must be a comma. That is, a variable definition must not be split between two cards.

If a vector variable is involved, the entire vector may be input by naming it and then listing as many values as there are vector elements. An example of a vector variable is NFLAG which contains 6 elements and is an integer variable. It may be input by punching NFLAG=3,3,3.

4,1,0, which sets NFLAG(1) to 3, NFLAG(2) to 3, etc. The same result may be obtained by punching NFLAG(1)=3, NFLAG(2)=3, etc., or NFLAG=3*3,4,1,0, where "3*3" is equivalent to 3,3,3.

1. Required Inputs

The following named variables are required inputs to the FORTRAN program.

APPD Distance in miles from the initial approach fix to the landing touchdown point.

APPSPD The mean approach speed of the aircraft, in MPH.

ARRT The initial mean time interval, in minutes, between arrivals at the holding pattern.



AVGATE The mean time required to load and unload passengers, measured in minutes.

DIST The number of miles of separation required between consecutive aircraft on the approach course.

LUPPER The upper limit for the table of transit times, units are time units.

LOWER The lower limit for the table of transit times in time units.

LINC The number of time units in each tabular interval in the table of transit times.

NGATES The number of passenger gates available in the terminal.

RUN The amount of time, in time units, to be simulated.

Statistics are kept for this time period unless a value for STDY is specified (see Optional Input section for STDY).

SPACE The number of miles of separation that is required between an arrival and a departure.

TDSPD The mean aircraft landing speed, in MPH.

TIMEU The number of seconds to be represented by each time unit.

WDIST The number of miles that must be traveled on a goaround to re-enter the approach course at the initial approach fix.



WOFFD The minimum distance, in miles from the touchdown point that a wave off can be safely initiated.

2. Optional Inputs

NFLAG

The following named variables are optional inputs to the FORTRAN program. The variables for which a default value is listed will be set to that default value if the user does not assign a value to them.

ACCEL The acceleration rate on takeoff, measured in ft/sec^2 . The default value is 10 ft/sec².

A six element vector used to flag options in specifying probability distributions. Three values are meaningful; 1, 2, and 3. The default value is 1. This variable is used to set up options for the following variables: ARRT, APPSPD, TDSPD, AVGATE, TAXIIN, and TAXIOU. The preceding list is ordered, i.e. NFLAG (1) refers to ARRT, NFLAG (2) to APPSPD, etc. Each time the simulation needs a value to use for one of these parameters (the actual inter arrival time between two aircraft, for example) it realizes a value from a probability distribution according to the following rules: If NFLAG is 1 (or default) a single value is realized with probability one. This value is the mean value, as input. If NFLAG is 2, a uniform distribution is sampled. If NFLAG is 3, a user specified distribution is sampled.



AMODIF

A six element vector used with NFLAG. If the corresponding NFLAG value is 1, AMODIF is ignored. If the corresponding NFLAG value is 2, the parent variable value (ARRT, APPSPD, TDSPD, etc.) is considered the mean, and the AMODIF value is half the range of the uniform distribution. That is, the distribution range is the mean + AMODIF. If the corresponding NFLAG value is 3, the AMODIF value is the number of points the user wishes to specify to define the function the simulation will use. The user then must supply the required number of function points to the GPSS program. To realize a value, the number assigned to the parent variable will be multiplied by the function value obtained.

TACCEL

The program normally computes the time to accelerate to takeoff speed on the basis of a constant acceleration at rate ACCEL from a standing start to landing speed. If this model is not satisfactory to the user, the number of time units required to accelerate can be input here.

CHANGE

The option exists to change the mean interarrival time periodically during the simulation. If this option is to be used, the number of time units between changes in mean interarrival time is input here. Note that RUN divided by CHANGE should result in a whole number.



DECEL The deceleration rate after landing, measured in ft/sec². The default value is 10 ft/sec².

This is a flag used to indicate that inclement
weather is to be simulated. A value of 1 indicates
this option is to be used. The result is the increasing of landing roll out by a factor of 1.1. A zero
indicates noninclement weather is to be simulated.
The default value is zero.

NPUNCH The logical value which is assigned to the unit to process punched output. The default value is 7, the normal IBM 360/67 punch code.

NWRITE The logical value which is assigned to the unit to process printed output. The default value is 6, the normal IBM 360/67 printer code.

NPFLAG This is a flag on aircraft transit time. A 1 specifies that each aircraft transit time is to be printed and tabulated. A zero specifies tabulation only. The default value is zero. This option should be used with caution. Each aircraft transit time printed out will result in three lines of output. This can easily lead to a large volume of paper.

STDY The option exists to keep statistics from other than the start of the run. Assigning a number to this variable specifies the number of time units from



the beginning of the run at which statistics will be started.

TAXIIN The mean number of minutes required to taxi from the runway to the passenger gate. The default is 2.0 minutes.

TAXIOU The mean number of minutes required to taxi from the passenger gates to the end of the runway. The default value is 2.0 minutes.

TDCEL The number of time units necessary to decelerate to taxi speed after landing. The default computes the time using a model of constant deceleration from landing speed to TURNOF (see below) at a rate of DECEL.

TURNOF The speed in MPH at which the aircraft can turn off
the runway after landing and deceleration. The
default value is 10 MPH.

WINDD The wind direction relative to the runway heading,
measured in degrees from zero to 180. The default
value is zero.

WINDS The wind speed in MPH. The default value is zero.

B. FORTRAN VARIABLES

The following list contains the principle FORTRAN variables and the rules and quantities used to compute them.



Variable formats are required for some outputs. The vectors which are used to contain these formats are: FMT, BLANK, SFMT, DIGIT, DIGIS, STG, TAB, TABR, FNCTS and Z1 through Z15.

HWIND The computed headwind component.

GSPEED The mean ground speed. It is computed by subtracting the headwind component from the mean approach speed.

COMIT The time before an arrival lands after which no more departures can be cleared ahead of him. It is computed by dividing the minimum allowable spacing between arrivals and departures by the mean ground speed.

ATIME The mean time required for an approach. It is obtained by dividing the approach distance by the mean ground speed.

IHX(1) The initial mean interarrival time converted to time units.

IXH(2) The mean time needed to obtain the required interarrival spacing on the approach course.

IXH(3) The mean time required to travel from the holding pattern to the commit point. The commit point is determined from the COMIT computation above.

IXH(4) The mean time required to travel from the commit point to the runway threshold.



- IXH(5) The mean time needed to travel from the threshold to the touchdown point.
- The time required to clear the runway after landing.
 It is computed by adding 5 seconds to the time required to decelerate after landing.
- IXH(7) The mean time required to taxi from the runway to the gate.
- IXH(8) The mean gate time.
- IXH(9) The mean time needed to taxi to the runway from the gate.
- IXH(10) The time needed to taxi from the end of the taxi way to position on the runway for takeoff.
- IXH(11) The time required to accelerate and takeoff.
- IXH(12) The time required to travel back to the start of the approach if a go-around is required.
- IXH(13) The time from which statistics are to be kept if other than from time zero.
- IXH(14) A flag to indicate if variable mean interarrival time is to be used.
- IXH(15) The mean interarrival time change interval. It is set equal to CHANGE.
- IXH(16) The number of gates to be simulated.
- CHANGE The time intervals at which changes in interarrival time are to be made.



The number of times the mean interarrival time is to be changed, if this option is used. It is computed by dividing RUN by CHANGE and subtracting 1 from the product.

The program uses two subroutines called "FITIT" and "FUNCTS".

These do format fitting and no other computations.

C. FORTRAN OUTPUT

IC

Appendix B contains a sample of the FORTRAN output. The printed output consists of two types, informational and directive.

The informational output gives the user a record of what the program has done. The first output produced is a copy of the values of all input variables. Some optional inputs which were not assigned values by the user may show negative values. This is normal and should not concern the user. The program will print a copy of all punched cards produced.

The program will check all 6 NFLAG values and their corresponding AMODIF values. If an NFLAG is specified 2 or 3, and no AMODIF value is assigned, the NFLAG will be set to 1. All NFLAG values after the check is made will be printed.

The directive output consists of instructions to supply data to the GPSS program. The data required will be a specified number of function points. All information is to be on punched cards. The program will specify the placement of the punched cards as "following card____" where the blank will contain a card number. The card numbers referred to are punched in columns 77-80 of the GPSS deck.



XII. PROCEDURES FOR GPSS RUN

This section contains the procedures the user should follow between the FORTRAN run and the GPSS run, as well as some general remarks about the programs.

A set of function points will be required for each user supplied probability function to be used (each NFLAG set to 3), and for mean interarrival time changes. For probability functions, the first number of the ordered pair specifying the function point is the independent variable. This will be realized from a uniform distribution. The range of the uniform distribution will be 0 to 1 for arrival rate, landing speed, gate time, taxi in time, and taxi out time. It will be 0 to 1000 for approach speed. The second number of the ordered pair is the value of the dependent variable at the function point which is being described.

For mean interarrival time changes, the first number of each pair is an integer from 1 to IC (RUN/CHANGE -1). The second number is the mean interarrival time for that time period.

Appendix B contains some examples of function definition cards included in the GPSS deck. All of these cards are punched starting in column 1 and not past column 72, with no imbedded blanks. As many cards as are necessary may be used. Ordered pairs are separated by the character /, and the numbers in each pair are separated by a comma. The last pair on each card is not followed by the character /. Decimal



points may be omitted for whole numbers. The pairs must be ordered among themselves so that the independent variable is monotone increasing.

An example would be; 1, 2.31/1.1,5/1.11,10.4/2,0.03.

The FORTRAN program will produce punched output which is to be included in the basic GPSS source deck. The cards will have numbers punched in columns 77-80 which indicate their relative position in the GPSS deck. If a like numbered card already exists in the basic GPSS deck, it is to be replaced by the new card. Otherwise, the new card is to be placed in the deck in numerical order. Gaps can be expected in the card numbering system. The GPSS deck should be restored to its original basic configuration as listed in Appendix A, before another run is set up.

The GPSS program will produce the same sequence of random numbers for each run. To obtain a different sequence of random numbers, a card punched starting in column 8 with the word RMULT, and punched starting in column 19 with 2 commas and a number, may be included in the GPSS deck. The number must be a seven digit or smaller, odd number, and will be the seed value for the GPSS random number generator. This card should be placed immediately following the SIMULATE card at the head of the GPSS deck. A different sequence of random numbers will be produced for each different RMULT number used.



APPENDIX A

SOURCE LISTINGS

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3 TABLE OF TRANSIT TIMES

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APPENDIX B

The following pages show the input and output for a sample run of the model.

The first page shows the input cards that were used. Next is the FORTRAN printed output followed by the punched output.

The GPSS source output shows the function definition cards that were included as per the instructions in the FORTRAN printed output.

The GPSS output has been edited to exclude the partially compiled source listing.



THE FOLLOWING INPUT CARDS WERE USED IN THE SAMPLE RUN.

&INPUT APPD=9.0, APPSPD=82.3, ARRT=5.45, AVGATE=3.0, DIST=2.0, LUPPER=324, LLCWER=156,LINC=12,NGATES=3,RUN=3600.,SPACE=1.0,TDSPD=77.,TIMEU=5.0, WDIST=13.0,WOFFD=0.1,NFLAG=3*3,1,3,1,AMODIF=23.0,2*29.0,0.,23.0,0., TAXIIN=1.5.TAXIGU=1.5.CHANG==360.,STDY=1440., SEND



FORTRAN PRINTED OUTPUT

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INITIAL XH3.36/XH9.18/XH10.3/XH11.2/XH12.97/XH13.1440/XH14.2
INITIAL XH3.360
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ADVANCE XH4.FN$FXH2 TRAVEL TO MAKEDEF POINT
ADVANCE XH4.FN$FXH2 TRAVEL TO MAKEDEF POINT
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aster's Thesis; September 1971			
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EPORT DATE	78. TOTAL NO	. OF PAGES	76. NO. OF REFS
ptember 1971	6	9	7
CONTRACT OR GRANT NO.	98. ORIGINATO	DR'S REPORT NO	UMBER(5)
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Determination of STOL air terminal traffic capacity through use of computer simulation.

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